

# Current Collapse Suppression by Gate Field-Plate in AlGa<sub>N</sub>/Ga<sub>N</sub> HEMTs Md.

メタデータ	言語: eng 出版者: 公開日: 2014-04-15 キーワード (Ja): キーワード (En): 作成者: Hasan, Md. Tanvir, Asano, Takashi, Tokuda, Hirokuni, Kuzuhara, Masaaki メールアドレス: 所属:
URL	<a href="http://hdl.handle.net/10098/8216">http://hdl.handle.net/10098/8216</a>

# Current Collapse Suppression by Gate Field-Plate in AlGaIn/GaN HEMTs

Md. Tanvir Hasan, *Student Member, IEEE*, Takashi Asano, Hirokuni Tokuda, and Masaaki Kuzuhara, *Fellow, IEEE*

**Abstract**—Current collapse measurements have been performed for AlGaIn/GaN HEMTs having identical breakdown voltages but with different field plate (FP) lengths. The results indicated that applying more positive on-state gate biases resulted in pronounced recovery in the dynamic on-resistance for the FP device, whereas no gate-bias effects were observed for the device without FP. The mechanism responsible for the reduced current collapse by FP is proposed, in which the key role is played during on-state by the quick field-effect recovery of partial channel depletion caused by electron trapping at AlGaIn surface states between gate and drain.

**Index Terms**—AlGaIn/GaN HEMT, field plate, on-resistance, current collapse.

## I. INTRODUCTION

AN AlGaIn/GaN-based high-electron-mobility transistor (HEMT) is considered as an excellent candidate for future power devices due to its high breakdown voltage, high saturation drain current, and low on-resistance ( $R_{on}$ ) [1], [2]. However, increased dynamic  $R_{on}$  by current collapse is regarded as one of the most critical issues to be solved for actual power-switching applications [3]-[4]. Various techniques have been reported as an effective approach to suppress current collapse, such as surface passivation [5], surface charge control with GaN cap layer [6], and field plate (FP) structure [7]-[10]. Saito *et al.* reported that the FP approach enhanced the breakdown voltage and hence suppressed the increase of dynamic  $R_{on}$  due to relaxation of electric field crowding at the gate edge in the drain side [9]. Brannick *et al.* reported by their computer simulation that FP was effective to reduce electron trapping by limiting tunneling injection of electrons into surface traps located in the gate-to-drain region [10]. Evidently, no experimental evidences have been identified to date with respect to the effect of FP on the dynamic switching performance of AlGaIn/GaN HEMTs.

In this letter, we report measurement results of dynamic  $R_{on}$  for a series of AlGaIn/GaN HEMTs with essentially the same breakdown voltage but with different FP lengths. Dramatic reduction in current collapse is presented for the FP device, in which trap-induced increase in the gate-to-drain access

resistance is quickly recovered by the field effect of positively biased FP electrode.

## II. DEVICE FABRICATION

The epitaxial structure used in this work was grown by MOCVD on a 4H-SiC substrate. It consists of a 500-nm GaN channel, and a 25-nm  $Al_{0.25}Ga_{0.75}N$  barrier. Hall-effect measurements showed a two-dimensional electron gas (2DEG) density of  $1.01 \times 10^{13} \text{ cm}^{-2}$  and an electron mobility of  $1500 \text{ cm}^2/\text{Vs}$ .

HEMT device fabrication began with mesa isolation using  $BCl_3/Cl_2$ -based inductively coupled plasma reactive ion etching. Source and drain ohmic contacts were formed by e-beam evaporation of Ti/Al/Mo/Au metal stacks, followed by rapid thermal annealing at  $850 \text{ }^\circ\text{C}$  for 30 s in a  $N_2$  atmosphere. A contact resistance of  $0.34 \text{ } \Omega\text{mm}$  was measured. Devices were then passivated with a 200-nm sputter-deposited SiN film. The gate window was opened by dry etching of the SiN film, followed by Schottky gate and FP formation with Ni/Au. The gate length, gate-to-source distance, and gate width were fixed at 3, 3, and  $100 \text{ } \mu\text{m}$ , respectively.

## III. DEVICE CHARACTERISTICS AND DISCUSSION

Essentially the same dc characteristics have been measured for devices with and without FP. With a gate-to-drain distance ( $L_{GD}$ ) of  $10 \text{ } \mu\text{m}$ , the maximum drain current defined at  $V_{GS}=1 \text{ V}$  was  $500 \text{ mA/mm}$  and the gate-to-drain leakage current was  $10^{-7} \text{ A/mm}$  measured at a bias voltage of  $200 \text{ V}$ .

Fig. 1 shows static  $R_{on}$  and breakdown voltage as a function of  $L_{GD}$  for devices without FP. The off-state source-to-drain breakdown voltage was defined at a drain current of  $0.1 \text{ mA/mm}$ . During the measurements, the back side of SiC substrate was kept floating. Almost the same dependence of static  $R_{on}$  and breakdown voltage on  $L_{GD}$  has been measured for devices with different FP length ( $L_{FP}$ ) of 1, 3, and  $5 \text{ } \mu\text{m}$ . Here, to avoid possible breakdown between FP and drain,  $L_{FP}$  of  $1 \text{ } \mu\text{m}$  was only tested for the device with  $L_{GD}=5 \text{ } \mu\text{m}$ . The static  $R_{on}$  and the breakdown voltage were in the range of  $9.5\text{-}10.7 \text{ } \Omega\text{mm}$  and  $700\text{-}740 \text{ V}$ , respectively, for devices with  $L_{GD}=10 \text{ } \mu\text{m}$ . The linear increase in the breakdown voltage, as shown in Fig. 1, suggests that the horizontal electric field would not be crowded

Manuscript received March 26, 2013.

M. T. Hasan, T. Asano, H. Tokuda and M. Kuzuhara are with the Graduate School of Engineering, University of Fukui, Bunkyo 3-9-1, Fukui 910-8507, Japan (email: tan\_vir\_bd@yahoo.com, kuzuhara@fuee.u-fukui.ac.jp).

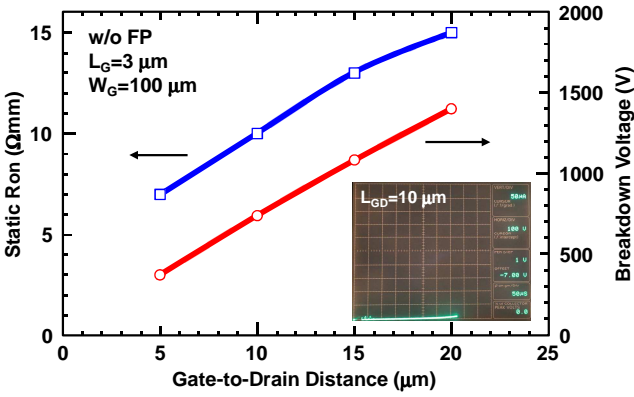


Fig. 1. Static on-resistance and breakdown voltage as a function of gate-to-drain distance ( $L_{GD}$ ) for AlGaIn/GaN HEMTs without field plate. Inset shows breakdown characteristics for the device with  $L_{GD}=10 \mu\text{m}$ .

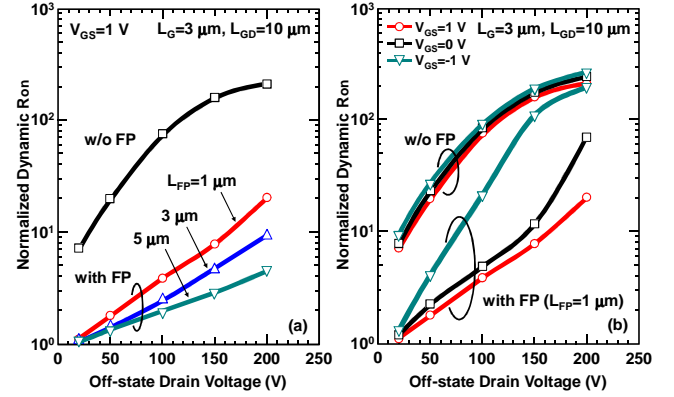


Fig. 3. Normalized dynamic on-resistance as a function of off-state drain bias voltage for AlGaIn/GaN HEMTs with and without FP. (a) Dependence of  $L_{FP}$  and (b) dependence of  $V_{GS}$ .

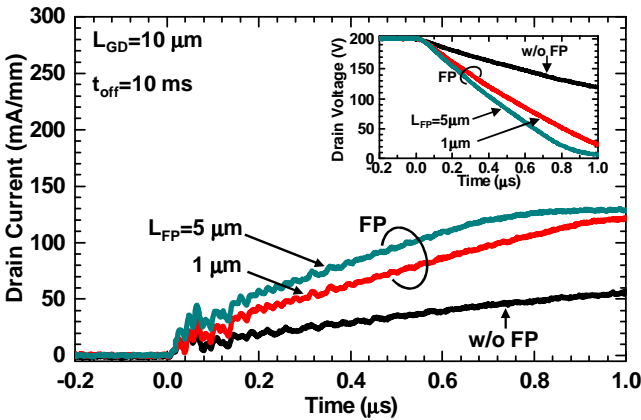


Fig. 2. Transient drain current of AlGaIn/GaN HEMTs with and without FP. Pulsed mode is operated with  $15 \text{ k}\Omega$  load line with off-state drain bias voltage of  $200 \text{ V}$ . Inset shows transient drain voltage.

near the gate edge. The virtual gate model [3] is a qualitative explanation for the increasing tendency of breakdown voltage with  $L_{GD}$ , but does not account for the linear increase with  $L_{GD}$  that we have observed between devices with different  $L_{FP}$ . Such linear increase in the breakdown voltage, as shown in Fig. 1, would be more reasonably explained if we assume a constant electric field distribution between gate and drain, even though direct experimental verification of field distribution has not yet been successfully made. Instead, our 2-dimensional device simulation (data not shown) suggested that uniform field distribution could be established when the surface negative charge was balanced with the positive polarization charge at the AlGaIn/GaN interface. The importance of balanced negative and positive polarization charges for establishing uniform field distribution has been proposed as a concept of natural super junction [11]. More work is needed to verify the possibility of forming uniform field distribution during off states by the presence of balanced negative and positive polarization charges on the front and back surfaces of AlGaIn.

Characterization of dynamic  $R_{on}$  was carried out by on-wafer pulsed measurements, where the gate voltage was switched from off-state ( $V_{GS}=-5 \text{ V}$ , below the threshold voltage of  $-3.7 \text{ V}$ ) to on-state ( $V_{GS}=1 \text{ V}$ ), while applying a drain bias voltage ( $V_{DS}$ )

up to  $200 \text{ V}$ . The load resistance ( $R_L$ ) was connected in series with the tested device and was adjusted so that  $R_{on}$  was reasonably measured in the linear region, i.e., below  $1/4$  of the maximum drain current. The on-state duration time ( $t_{on}$ ) and the off-state duration time ( $t_{off}$ ) were fixed at  $1 \mu\text{s}$  and  $10 \text{ ms}$ , respectively. The transient output current was measured by a current probe (LeCroy CP030). Fig. 2 shows measured time-dependent waveforms of the drain current and the drain voltage (inset) of devices with and without FP. A constant  $R_L$  of  $15 \text{ k}\Omega$  was used at  $V_{DS}=200 \text{ V}$ . Although the drain current waveform exhibited an oscillatory response in the early stage (up to  $200 \text{ ns}$ ), our setup was able to stably measure the drain current response with a time constant of more than  $300 \text{ ns}$ . The measurement accuracy of on-state current was about  $\pm 0.03 \text{ mA}$  and that of voltage was less than  $\pm 0.1 \text{ V}$ . The device without FP exhibited seriously degraded drain current response with a long time constant (more than  $1 \text{ ms}$ ), while the drain current recovery was much faster for the FP device. The dynamic  $R_{on}$  measured at  $t_{on}=1 \mu\text{s}$  was as large as  $2220 \Omega\text{mm}$  for the device without FP, while that for the FP device ( $L_{FP}=5 \mu\text{m}$ ) was only  $45 \Omega\text{mm}$ . More interestingly, the drain current recovery became faster as  $L_{FP}$  was increased, indicating that the gate-FP structure with reasonably long  $L_{FP}$  is effective to reduce dynamic  $R_{on}$ .

To represent the magnitude of current collapse quantitatively, we have defined the normalized dynamic  $R_{on}$ , where the  $R_{on}$  value measured at  $t_{on}=1 \mu\text{s}$  was normalized by its static value. For devices without FP, the normalized dynamic  $R_{on}$  was gradually increased from  $190$  to  $320$  with increasing  $L_{GD}$  from  $5$  to  $20 \mu\text{m}$ . Fig. 3 (a) shows the normalized dynamic  $R_{on}$  as a function of off-state  $V_{DS}$  with  $V_{GS}=1 \text{ V}$ . It is obvious that the dynamic  $R_{on}$  increases with increasing  $V_{DS}$ . Note that the normalized dynamic  $R_{on}$  for the FP device is lowered by 1 or 2 orders of magnitude as compared to the device without FP, indicating that only reducing the exposed-access distance (i.e.,  $L_{GD}-L_{FP}$ ) is not enough for significant current collapse reduction. These results demonstrate a primary advantage of FP to suppress current collapse. To our knowledge, this is the first report showing experimental evidence of current collapse suppression by using gate FP, where the dynamic  $R_{on}$  was compared among devices with essentially the same breakdown

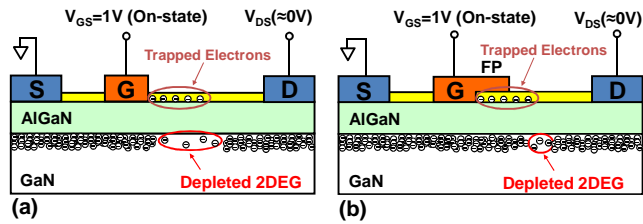


Fig. 4. Schematic diagrams of on-state device operation for AlGaIn/GaN HEMTs (a) without FP and (b) with FP.

voltages. Fig. 3 (b) shows normalized dynamic  $R_{on}$  as a function of  $V_{DS}$  with different  $V_{GS}$ . For the device without FP, the normalized dynamic  $R_{on}$  was increased with increasing  $V_{DS}$ , approaching more than 200 at  $V_{DS}=200$  V. This behavior was almost independent of the on-state  $V_{GS}$  between -1 and +1 V. On the other hand, for the FP device,  $V_{GS}$  dependence was clearly observed, where normalized dynamic  $R_{on}$  was significantly reduced by increasing on-state  $V_{GS}$  from negative to positive values due to generation of capacitively-induced additional channel charge (on the order of  $10^{11}$  cm $^{-2}$ ) in the early stage of on states (up to  $t_{on}=1$   $\mu$ s). Note that the normalized dynamic  $R_{on}$  of the FP device with  $V_{GS}=-1$  V is approaching to that for the device without FP, indicating that FP electrode becomes less effective on dynamic  $R_{on}$  when on-state  $V_{GS}$  was set at negative values under high  $V_{DS}$  conditions.

Fig. 4 shows the schematic diagram of device operation under on states for AlGaIn/GaN HEMTs with and without FP. During off state with  $V_{GS}=-5$  V, both devices are considered essentially the same, where channel 2DEG electrons are fully depleted under the gate. Due to strong reverse electric fields between gate and drain during off states, electrons are injected from the gate edge as leakage currents and are assumed to be trapped at the AlGaIn/SiN interface. Hence, higher drain bias voltages lead to enhancement of trapped electrons [12]. Those trapped electrons contribute to partly deplete the channel 2DEG electrons near the gate edge in the drain side. Next the gate voltage is switched to on state ( $V_{GS}=1$  V), resulting in quick generation of electron accumulation under the gate. However, emission of captured electrons does not occur within a short period of time (i.e., less than 1  $\mu$ s). Hence it takes rather a long time before steady-state condition is reached for the device without FP (see Fig. 4 (a)). This is the main reason for causing the current collapse. On the other hand, the situation for the FP device is quite different, as shown in Fig. 4 (b). Since the AlGaIn surface near the gate is covered with FP, the partial depletion of 2DEG electrons can be instantly recovered by the field effect of the positively-biased FP electrode. Therefore, the recovery of channel electrons is much faster for the FP device, leading to more enhanced improvements in dynamic performance during on states with more positive gate biases, as shown in Fig. 3 (b).

#### IV. CONCLUSION

We have studied the effect of gate FP on current collapse for a series of AlGaIn/GaN HEMTs having essentially the same breakdown voltage but with different FP lengths. By applying a

more positive on-state gate bias voltage, pronounced recovery in the dynamic on-resistance was observed for the FP device, whereas no significant gate-bias effects were observed for the device without FP. The mechanism responsible for the improved current collapse was proposed, where field-effect charge control by FP resulted in the quick recovery of partial channel depletion in the gate-to-drain access region.

#### ACKNOWLEDGMENT

This work was performed as a part of the project named "Development of Nitride-based Semiconductor Crystal Substrate and Epitaxial Growth Technology" by NEDO.

#### REFERENCES

- [1] S. C. Binari, K. Ikossi, J. A. Roussos, W. Kruppa, D. Park, H. B. Dietrich, D. D. Koleske, A. E. Wickenden, and R. L. Henry, "Trapping effects and microwave power performance in AlGaIn/GaN HEMTs," *IEEE Trans. Electron Devices*, vol. 48, no. 3, pp. 465–471, Mar. 2001.
- [2] R. Chu, A. Corrión, M. Chen, R. Li, D. Wong, D. Zehnder, B. Hughes, and K. Boutros, "1200-V normally off GaN-on-Si field-effect transistors with low dynamic ON-resistance," *IEEE Electron Device Lett.*, vol. 32, no. 5, pp. 632–634, May 2011.
- [3] R. Vetry, N. Q. Zhang, S. Keller, and U. K. Mishra, "The impact of surface states on the DC and RF characteristics of AlGaIn/GaN HFETs," *IEEE Trans. Electron Devices*, vol. 48, no. 3, pp. 560–566, Mar. 2001.
- [4] W. Saito, T. Nitta, Y. Kakiuchi, Y. Saito, K. Tsuda, I. Omura, and M. Yamaguchi, "Suppression of dynamic On-resistance increase and gate charge measurements in high-voltage GaN-HEMTs with optimized field-plate structure," *IEEE Trans. Electron Devices*, vol. 54, no. 8, pp. 1825–1830, Aug. 2007.
- [5] B. M. Green, K. K. Chu, E. M. Chumbes, J. A. Smart, J. R. Shealy, and L. F. Eastman, "The effect of surface passivation on the microwave characteristics of undoped AlGaIn/GaN HEMTs," *IEEE Electron Device Lett.*, vol. 21, no. 6, pp. 268–270, Jun. 2000.
- [6] T. Kikkawa et al., "Surface charge controlled AlGaIn/GaN-power HEFT without current collapse and  $g_m$ ," in *IEDM Tech. Dig.*, 2001, pp. 25.4.1 - 25.4.4.
- [7] Y. Ando, Y. Okamoto, H. Miyamoto, T. Nakayama, T. Inoue, and M. Kuzuhara, "10-W/mm AlGaIn-GaN HFET with a field modulating plate," *IEEE Electron Device Lett.*, vol. 24, no. 5, pp. 289–291, May 2003.
- [8] Y. Wu, A. Saxler, M. Moore, R. P. Smith, S. Sheppard, P. M. Chavarkar, T. Wisleder, U. K. Mishra, and P. Parikh, "30W/mm GaN HEMTs by field plate optimization," *IEEE Electron Device Lett.*, vol. 25, no. 3, pp. 117–119, Mar. 2004.
- [9] W. Saito, Y. Kakiuchi, T. Nitta, Y. Saito, T. Noda, H. Fujimoto, A. Yoshioka, T. Ohno, and M. Yamaguchi, "Field-plate structure dependence of current collapse phenomena in high-voltage GaN-HEMTs," *IEEE Electron Device Lett.*, vol. 31, no. 7, pp. 659–661, Jul. 2010.
- [10] A. Brannick, N. A. Zakhleniuk, B. K. Ridley, J. R. Shealy, W. J. Schaff, and L. F. Eastman, "Influence of field plate on the transient operation of the AlGaIn/GaN HEMT," *IEEE Electron Device Lett.*, vol. 30, no. 5, pp. 436–438, May 2009.
- [11] H. Ishida, D. Shibata, M. Yanagihara, Y. Uemoto, H. Matsuo, T. Ueda, T. Tanaka, and D. Ueda, "Unlimited high breakdown voltage by natural super junction of polarized semiconductor," *IEEE Electron Device Lett.*, vol. 29, no. 10, pp. 1087–1089, Oct. 2008.
- [12] Z. Tang, S. Huang, Q. Jiang, S. Liu, C. Liu, and K. J. Chen, "High-voltage (600-V) low-leakage low-current-collapse AlGaIn/GaN HEMTs with AlN/SiN $_x$  passivation," *IEEE Electron Device Lett.*, vol. 34, no. 3, pp. 366–368, Mar. 2013.